Microscopic modeling and direct simulation of active suspensions

A. Decoene, S. Martin, B. Maury

Laboratoire de Mathématiques Université Paris - Sud

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Introduction : from individual to collective dynamics

A simple microscopic model : pointlike particles

A model for chemotaxis

An accurate microscopic model : rigid particles

Ongoing work and perspectives

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Active suspensions

Bacteria : E. Coli [Berg, 1983] ($\sim 2 \mu m \times 0.5 \mu m$)



Green algae : Chlamydomonas (radius $\sim 10 \ \mu m$)



life at low Reynolds number ($Re \ll 1$) : viscous forces dominate !

Self-propulsion in Stokes flow

Pushers : bacteria *E. coli, B. Subtilis*

 helical flagella localized on the surface, responsible of propulsion

Pullers : Chlamydomonas

 two cilia performing non-reversible breast stroke





 \longrightarrow capable of swimming many cell-lengths per second

 \longrightarrow long-range perturbation of the flow (decreases as $O(\frac{1}{r})$ in 2D, $O(\frac{1}{r^2})$ in 3D)

Chemotaxis



 \longrightarrow on a long time scale each swimmer performs a random walk with a bias towards favorable direction

Collective dynamics

Coherent structures [Cisneros et al. '07], [Aranson et al. '07], ...

- self-organized coherent structures with the spatial scale exceeding the size of an individual swimmer
- collective velocity greater than the individual velocity
- weakly turbulent appearance of the flow: recirculations, vortices...

 \longrightarrow enhanced transport and mixing of particles, can be essential for nutriments resupplying

Impact of active particles on the viscosity of the suspension

- ▶ experiments [Sokolov & Aranson '07], [Rafaï *et al.*'10]
- analytical and numerical studies [Pedley '07], [Berlyand et al.'08], [Shelley et al.'09]

Motility can strongly modify the effective viscosity of a suspension

Chemotaxis [Tuval et al.'05]

- bioconvection >
- hydrodynamic instabilities >I

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A simple model (1)

Swimmers are modelled as point particles $i_{i=1...N}$ in a fluid domain Ω , \boldsymbol{u} and p velocity and pressure in the fluid \boldsymbol{x}_i and θ_i position and orientation of swimmer i

• Equilibrium of forces and torque on each body :

$$F_{drag} + F_{prop} + F_{buoy} = 0$$

 $G = 0$

► Stokes flow :

$$-\mu \Delta \boldsymbol{u} + \boldsymbol{\nabla} \boldsymbol{p} = \sum_{i=1...N} - \boldsymbol{F}_{drag,i} \, \delta_{x_i} - \boldsymbol{F}_{prop,i} \, \delta_{y_i}$$
$$= \sum_{i=1...N} \boldsymbol{F}_{buoy} \delta_{x_i} + \boldsymbol{F}_{prop} (\delta_{x_i} - \delta_{y_i})$$

A simple model (2)

► Fluid :

$$\begin{cases} -\mu \Delta \boldsymbol{u} + \boldsymbol{\nabla} \boldsymbol{p} &= \boldsymbol{f}_f & \text{in } \boldsymbol{\Omega} \\ \boldsymbol{\nabla} \cdot \boldsymbol{u} &= \boldsymbol{0} & \text{in } \boldsymbol{\Omega} \end{cases}$$

with $\mathbf{f}_{f} = \sum_{i=1...N} \mathbf{F}_{buoy} \chi_{i}$ (only first order contributions, regularization of dirac)

Particle dynamics :

Faxen's law for spherical rigid bodies (radius a)

$$(\dot{\boldsymbol{x}}_i - \boldsymbol{u}(\boldsymbol{x}_i)) = \frac{1}{6\pi\mu a} \left(-\pi\mu a^3 \Delta \boldsymbol{u}(\boldsymbol{x}_i) + \boldsymbol{F}_{buoy} + \boldsymbol{F}_p \right)$$
$$\dot{\theta}_i = \frac{1}{2} (\boldsymbol{\nabla} \times \boldsymbol{u})(\boldsymbol{x}_i)$$

► Dealing with congestion :

Finite size of particles is taken into account in order to compute non-elastic collisions.

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A model for chemotaxis

Tumbling : Poisson process

 $T_{run} = {
m duration}$ of a ${
m Run} \sim \exp(\lambda)$

 $\lambda =$ Tumbling frequency : variable !

heta= new orientation \sim $U(0,2\pi)$

► first model :

$$\lambda(c) = 1 - \epsilon \operatorname{Signe}\left(rac{Dc}{Dt}
ight), \quad \epsilon < 1$$

▶ a finer model ("memory" of the swimmer) : [Locsei, 2007] :

$$\lambda(c) = 1 - \epsilon \operatorname{Signe}\left(\int_{t-\Delta t}^{t} c(s) g(t-s) ds\right)$$

where g(s)=1 si $s\leq \Delta t/4$ et g(s)=-1/3 si $s>\Delta t/4$

A model for chemotaxis

Interaction with oxygen (oxygentaxis)

 $1. \ \mbox{Convection-diffusion}$ equation for oxygen :

$$\partial_t c + \boldsymbol{u} \cdot \boldsymbol{\nabla} c - D_c \Delta c = -\kappa f(c) \chi_B \quad dans \ \Omega$$
.

$$\begin{array}{l} c: \text{ oxygen concentration in the fluid,} \\ \kappa: \text{ consuming rate} \\ f(c): \text{ modulation of the rate } (\rightarrow \ 0 \text{ when } c \rightarrow 0, \rightarrow 1 \text{ when } c \rightarrow +\infty). \end{array}$$

2. Modulation of the propulsion force intensity :

$$f_p \longrightarrow 0$$
 when $c \longrightarrow 0$

Simulating bioconvective phenomena

mise en évidence d'instabilités hydrodynamiques dues au gradient de densité

93/100





Simulating bioconvective phenomena

in a droplet (after the experiment by *Goldstein e.a., 2005*): boycott effect + hydrodynamic instabilities

88/100





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Full microscopic model

- Each swimmer = rigid ellipsoidal particle B + associated region in the fluid P (representing cilia or flagellar bundle) (not rigid !)
- Selfpropulsion : force of magnitude f_P and direction τ acting on the fluid in region P and on the cell in B (in opposite direction !)



Isolated swimmer (force-free) : $\boldsymbol{F}_{p} = -f_{p} \boldsymbol{\tau} = -\boldsymbol{F}_{b}$

Volumic forces :
$$F_p = \int_P f_p \, dx$$
, $F_b = \int_B f_b \, dx$

Fluid-structure interaction problem

Notations:

 $\Omega \subset \mathbb{R}^2 {:}$ bounded and regular domain,

 $(B_i)_{i=1...N}$: rigid inclusions in Ω , denoting the bodies of the swimmers,

$$B = \bigcup_{i=1...N} B_i \text{ rigid domain,}$$



 x_i coordinates of the center of mass of B_i ,

 θ_i angle defining the position of the flagellum of B_i ,

$$\boldsymbol{V} = (\boldsymbol{V}_i = \dot{\boldsymbol{x}}_i) \in \mathbb{R}^{2N},$$

$$\omega = (\omega_i = \dot{\theta}_i) \in \mathbb{R}^N.$$

Fluid-structure interaction problem

Notations:

- $\begin{array}{ll} ({\bm u},{\bm p}) & \mbox{velocity and pressure fields defined in } \Omega \setminus \bar{B} \\ ({\bm V},\omega) & \mbox{translational and rotational velocities of swimmers} \end{array}$
- Stokes fluid:

$$\begin{cases} -\mu \Delta \boldsymbol{u} + \boldsymbol{\nabla} \boldsymbol{p} = \boldsymbol{f}_{f} := \sum_{i=1}^{N} \boldsymbol{f}_{p_{i}} \chi_{P_{i}} & \text{in } \Omega \setminus \bar{B}, \\ \boldsymbol{\nabla} \cdot \boldsymbol{u} = 0 & \text{in } \Omega \setminus \bar{B}, \\ \boldsymbol{u} = 0 & \text{on } \partial\Omega, \\ \boldsymbol{u} = \boldsymbol{V}_{i} + \omega_{i} (\boldsymbol{x} - \boldsymbol{x}_{i})^{\perp} & \text{on } \partial B_{i}, \forall i. \end{cases}$$

Forces equilibrium (Newton's second law of motion):

$$\begin{cases} \int_{B_i} \boldsymbol{f}_{b_i} - \int_{\partial B_i} \boldsymbol{\sigma} \cdot \boldsymbol{n} = 0, \quad \forall i, \\ \int_{B_i} (\boldsymbol{x} - \boldsymbol{x}_i)^{\perp} \cdot \boldsymbol{f}_{b_i} - \int_{\partial B_i} (\boldsymbol{x} - \boldsymbol{x}_i)^{\perp} \cdot (\boldsymbol{\sigma} \cdot \boldsymbol{n}) = 0, \quad \forall i. \end{cases}$$

The problem comes to minimize the functional

$$J(\tilde{\boldsymbol{u}}) = \mu \int_{\Omega} |\mathbb{D}(\tilde{\boldsymbol{u}})|^2 - \int_{\Omega} \boldsymbol{f} \cdot \tilde{\boldsymbol{u}}$$

on the subspace :

$${\it K}_{0}\cap{\it K}_{
abla}=ig\{{\it u}\in{\it H}_{0}^{1}(\Omega)\ /\ {m
abla}\cdot{\it u}=0,\ \mathbb{D}({\it u})=0\ {\it a.e.}\ {\it on}\ Big\}$$

with

$$\boldsymbol{f} = \sum_{i=1}^{N} \left(\boldsymbol{f}_{b_i} \chi_{B_i} + \boldsymbol{f}_{p_i} \chi_{P_i} \right).$$

 \rightarrow strong coupling of the problems on fluid and particles, without direct estimation of $\sigma \cdot n$.

Fictitious domain approach, in order to work with fixed cartesian meshes

In 2D : Penalty method ([Peyla '04], [Lefebvre '05], ...) leads to unconstrained spaces:

Let $\varepsilon > 0$ be small (inverse of the "viscosity" of the solid phase)

Minimization problem is approached by a modified minimization problem :

$$\begin{cases} \boldsymbol{u} \in K_{\nabla} \cap K_{\theta} \\ J(\boldsymbol{u}) = \min_{\tilde{\boldsymbol{u}} \in K_{\nabla} \cap K_{\theta}} J(\tilde{\boldsymbol{u}}) \end{cases} \approx \begin{cases} \boldsymbol{u}_{\epsilon} \in K_{\nabla} \\ J_{\epsilon}(\boldsymbol{u}_{\epsilon}) = \min_{\tilde{\boldsymbol{u}} \in K_{\nabla}} J_{\epsilon}(\tilde{\boldsymbol{u}}) \end{cases}$$

where

$$J_{\epsilon}(\tilde{\boldsymbol{u}}) = J(\tilde{\boldsymbol{u}}) + \frac{1}{\epsilon} \int_{B} |\mathbb{D}(\tilde{\boldsymbol{u}})|^2$$

Proposition.

$$oldsymbol{u}_\epsilon \longrightarrow oldsymbol{u}$$
 when $oldsymbol{\epsilon} \longrightarrow 0$ and $\exists C > 0$ such that $\mid oldsymbol{u}_\epsilon \ - \ oldsymbol{u} \mid \leq C \epsilon$

Fictitious domain approach, in order to work with fixed cartesian meshes

► In 2D : Penalty method

In 3D : this penalty method is not efficient : bad conditioning of matrix so that only direct methods can be used + non-optimal convergence rate.

Ongoing work (B. Fabrèges and B. Maury) : **fast 3D solver** for fluid - rigid particles interaction based on an optimal order fictitious domain method. **Updating positions and orientations** by evaluating V_i and ω_i and solving :

 $\boldsymbol{x}_i^{n+1} = \boldsymbol{x}_i^n + \Delta t \, \boldsymbol{V}_i, \qquad \theta_i^{n+1} = \theta_i^n + \Delta t \, \omega_i.$

Contacts :

In principle no contact in finite time.

In practice (time discretization, inexact estimate of lubrication forces) : contact or overlapping between bodies may occur.

Contact algorithm : robust handling relying on purely non-elastic collisions.

= projection of the velocities on a space of "admissible velocities" (based on a granular flow approach [Maury '06])

Algorithm | Contact handling



Figure: The contact algorithm applied to a set of circles

Algorithm | Contact handling



Figure: The contact algorithm applied to a set of ellipses



Figure: Pusher in a fluid at rest



Figure: Puller in a fluid at rest



Figure: No pusher side by side



Figure: ITwo puller side by side

PUSHER

VELOCITY FIELD AND BACTERIAL DISTRIBUTION - 50/100

Figure: Dense suspension (solid fraction : 30%)

PULLER

VELOCITY FIELD AND BACTERIAL DISTRIBUTION - 58/100

Figure: Dense suspension (solid fraction : 30%)



Correlation length of collective motion can exceed the size of individual cells by more than an order of magnitude.

- weak turbulence
- persistence of coherent structures

▶ ▶

Velocity correlation

$$\begin{split} \mathcal{I}(r,t) &:= \frac{\left\langle \boldsymbol{u}(\boldsymbol{x},t) \cdot \boldsymbol{u}(\boldsymbol{x}+re^{i\theta},t) \right\rangle_{\boldsymbol{x},\theta} - \left\langle \boldsymbol{u}(\boldsymbol{x},t) \right\rangle_{\boldsymbol{x}}^{2}}{\left\langle \boldsymbol{u}(\boldsymbol{x},t)^{2} \right\rangle_{\boldsymbol{x}} - \left\langle \boldsymbol{u}(\boldsymbol{x},t) \right\rangle_{\boldsymbol{x}}^{2}} \\ \mathcal{J}(\boldsymbol{x},t) &:= \frac{\left\langle \boldsymbol{u}(\boldsymbol{x},s) \cdot \boldsymbol{u}(\boldsymbol{x},s+t) \right\rangle_{\boldsymbol{s}}}{\left\langle \boldsymbol{u}(\boldsymbol{x},s)^{2} \right\rangle_{\boldsymbol{s}}} \end{split}$$



Figure: Space correlation functions for suspensions of pushers (left) and pullers (right)

- constant size of coherent structures already reached for $\phi = 8\%$
- $\blacktriangleright\,$ typical size \sim 5 times particle size



Figure: Time correlation functions for suspensions of pushers (left) and pullers (right)

Numerical results (2/4) | Hydrodynamics: collective dynamics



average velocity increases with the solid fraction above a critical concentration it decreases, due to congestion.

Rheology

Effective viscosity:

- resistance of a fluid which is being deformed by a shear stress
- macroscopic observable quantity measured by a rheometer:



Effective viscosity

Forces exerted by the fluid on the walls:

$$F_{|y=+a} = \int_{y=+a} \mathbf{e}_x \cdot \sigma \cdot (-\mathbf{e}_y), \quad F_{|y=-a} = \int_{y=-a} \mathbf{e}_x \cdot \sigma \cdot (+\mathbf{e}_y)$$

▶ In case of a Newtonian fluid, the exact solution is

$$\boldsymbol{u}(x,y) = -S\frac{y}{a}\mathbf{e}_x, \qquad p(x,y) = 0,$$

we have

$$F_0 := F_{|y=+a} - F_{|y=-a} = 2\mu \frac{S}{a}L$$

~

▶ Therefore, the effective viscosity can be defined as

$$\mu_{\text{eff}} = \frac{a}{2LS}F_0, \quad \text{with } F_0 := \int_{\{y=+a\}\cup\{y=-a\}} \mathbf{e}_x \cdot \sigma \cdot (-\mathbf{e}_y)$$

Effective viscosity : PUSHERS







Figure: Active suspension (I.) vs passive suspension (r.)

Effective viscosity : PULLERS







Figure: Active suspension (I.) vs passive suspension (r.)

Effective viscosity : PULLERS







Figure: Active suspension (I.) vs passive suspension (r.)

Effective viscosity : PULLERS







Figure: Active suspension (I.) vs passive suspension (r.)

Effective viscosity



Figure: Effective viscosity η/η_0 with respect to the solid fraction

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Phd work by Loic Lacouture (Paris Sud)

- Numerical analysis of the FE solution of elliptic problems with singular source term :
 - ► Solution of Stokes equations with dirac mass source term (2d and 3d) → singular solution → does not enter in the classical framework of finite element solutions for elliptic problems.
 - Numerical analysis shows that the convergence rate is not optimal.
 - Development of a numerical method allowing to recover the optimal convergence rate by extracting the singularity.
- Application to the micro-swimmer model :
 - ▶ Cilia and flagella can be seen as one-dimensional (infinitely thin) structures in a 3d flow in the asymptotic : thickness $\epsilon \rightarrow 0$ while the resultant force F_{hydro} they apply on the fluid remains constant.

Representing cilia and flagella

Prescribed description of the position of the cilium \to hydrodynamic force ${\it f}$ deduced using slender body theory

Here : mathematical formulation of the tracheal cilium beat cycle given by Fulford and Blake (1986)

We solve :

$$\begin{aligned} -\mu \Delta \boldsymbol{u} + \boldsymbol{\nabla} \boldsymbol{p} &= \boldsymbol{f} \delta_{\boldsymbol{S}} \\ \boldsymbol{\nabla} \cdot \boldsymbol{u} &= \boldsymbol{0} \end{aligned}$$

with f density of force distributed over the cilium.



3D simulations (B. Fabreges, PhD supervised by B. Maury) ►

Thank you for your attention